APPENDIX "D" - HYDRA FLOW MODEL - 1990
PART 2

LINE T AT DEVONSHIRE & GILBERT

Lateral length= 1 Upstream length= 1

*** CALHOUN PLACE Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
6	328	8	598.40	0.0057	0.1	0.0	1.66	0.11	18.85		
			596.54		0.0	0.0	0.33		0.58		
7	342	8	596.54	0.0152	0.1	0.0	2.39	0.11	11.53		
			591.35		0.0	0.0	0.27		0.95		

Lateral length= 670 Upstream length= 670

*** BUENA VISTA LATERAL Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
8	313	8	591.35	0.0028	0.1	0.0	1.25	0.09	22.91		
			590.46		0.0	0.0	0.37		0.41		

Lateral length= 313 Upstream length= 314

*** DEVONSHIRE LATERAL Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
9	325	10	595.17	0.0118	0.2	0.0	2.39	0.15	10.12		
			591.32		0.0	0.0	0.26		1.53		
10	168	10	591.32	0.0051	0.2	0.0	1.76	0.17	16.61		
			590.46		0.0	0.0	0.31		1.01		
11	324	10	590.46	0.0021	0.3	0.0	1.50	0.27	41.77		
			589.77		0.0	0.0	0.51		0.65		
12	338	10	589.77	0.0060	0.3	0.0	2.19	0.28	25.93		
			587.75		0.0	0.0	0.39		1.09		
13	321	10	587.75	0.0089	0.3	0.0	2.54	0.29	22.19		
			584.89		0.0	0.0	0.36		1.33		
14	330	10	584.89	0.0107	0.3	0.0	2.71	0.30	20.59		
			581.36		0.0	0.0	0.35		1.45		

LINE T AT DEVONSHIRE & GILBERT

*** DEVONSHIRE LATERAL — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
15	53	10	581.36	-0.0064	0.3	0.0	0.00	0.30	999.99	0.00	0
			581.70		0.0	0.0	0.00		0.00		0
16	325	10	581.70	0.0011	0.3	0.0	1.25	0.30	63.40		
			581.33		0.0	0.0	0.65		0.47		
17	334	10	581.33	0.0069	0.3	0.0	2.39	0.32	27.42		
			579.04		0.0	0.0	0.41		1.16		
18	333	10	579.04	0.0070	0.3	0.0	2.44	0.33	28.43		
			576.70		0.0	0.0	0.41		1.18		
19	330	10	576.70	0.0071	0.4	0.0	2.55	0.39	32.69		
			574.35		0.0	0.0	0.45		1.19		

Lateral length= 3182 Upstream length= 3497

*** CENTRAL LATERAL — Diversion

Link	Invert Up/Dn		Maximum Flow Values San	Inf	Sto	Mis	Design	Cost
21	Unknown	Discharge :	0.06	0.00	0.00	0.00	0.06	0
	Unknown	Diverted :	0.00	0.00	0.00	0.00	0.00	
		Incoming :	0.06	0.00	0.00	0.00	0.06	

*** CENTRAL LATERAL — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
22	331	8	601.29	0.0044	0.1	0.0	1.31	0.06	12.56		
			599.85		0.0	0.0	0.28		0.51		
23	162	8	594.52	0.0020	0.1	0.0	1.07	0.09	24.76		
			594.20		0.0	0.0	0.38		0.34		
24	169	8	594.20	0.0051	0.1	0.0	1.62	0.11	20.77		
			593.34		0.0	0.0	0.35		0.55		
25	333	8	593.32	0.0122	0.1	0.0	2.22	0.11	13.41		
			589.26		0.0	0.0	0.28		0.86		

LINE T AT DEVONSHIRE & GILBERT

*** CENTRAL LATERAL — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
26	327	8	589.24	0.0092	0.1	0.0	2.00	0.11	15.41		
			586.22		0.0	0.0	0.30		0.74		
27	327	8	586.28	0.0094	0.1	0.0	2.04	0.12	16.16		
			583.21		0.0	0.0	0.31		0.75		
28	329	10	583.23	0.0088	0.2	0.0	2.12	0.15	11.45		
			580.32		0.0	0.0	0.27		1.32		
	Lateral length=		1978		Upstream length=				1978		

*** MAYBERRY DIVERSION — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
29	311	8	601.29	0.0031	0.0	0.0	0.00	0.00	0.00		
			600.31		0.0	0.0	0.00		0.43		
30	362	8	600.31	0.0042	0.0	0.0	0.00	0.00	0.00		
			598.79		0.0	0.0	0.00		0.50		
	Lateral length=		673		Upstream length=				673		

*** ACACIA LATERAL — Diversion

Link	Invert Up/Dn		Maximum Flow Values San	Inf	Sto	Mis	Design	Cost
32	598.79	Discharge :	0.06	0.00	0.00	0.00	0.06	0
	598.79	Diverted :	0.00	0.00	0.00	0.00	0.00	
		Incoming :	0.06	0.00	0.00	0.00	0.06	

*** ACACIA LATERAL — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
33	330	8	598.79	0.0057	0.1	0.0	1.42	0.06	9.80		
			596.92		0.0	0.0	0.25		0.58		

LINE T AT DEVONSHIRE & GILBERT

*** ACACIA LATERAL Diversion

Link	Invert Up/Dn		Maximum Flow Values San	Inf	Sto	Mis	Design	Cost
35	596.92	Discharge :	0.07	0.00	0.00	0.00	0.07	0
	596.92	Diverted :	0.00	0.00	0.00	0.00	0.00	
		Incoming :	0.07	0.00	0.00	0.00	0.07	

*** ACACIA LATERAL Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
36	334	8	596.92	0.0041	0.1	0.0	1.28	0.07	13.38		
			595.56		0.0	0.0	0.28		0.49		
37	330	8	595.56	0.0067	0.1	0.0	1.60	0.08	11.91		
			593.35		0.0	0.0	0.27		0.63		
38	340	8	593.35	0.0070	0.1	0.0	1.67	0.08	12.94		
			590.97		0.0	0.0	0.28		0.65		
39	329	8	590.97	0.0077	0.1	0.0	1.73	0.08	12.37		
			588.45		0.0	0.0	0.27		0.68		
40	329	8	588.45	0.0097	0.1	0.0	2.00	0.11	13.84		
			585.25		0.0	0.0	0.29		0.76		
41	349	8	585.25	0.0109	0.1	0.0	2.28	0.15	18.50		
			581.46		0.0	0.0	0.33		0.81		
42	279	8	581.46	0.0093	0.1	0.0	2.16	0.15	19.95		
			578.86		0.0	0.0	0.34		0.75		
43	8	8	578.86	0.0013	0.1	0.0	1.09	0.15	53.77		
			578.85		0.0	0.0	0.59		0.28		

Lateral length= 2628 Upstream length= 3301

*** JUANITA DIVERSION Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove
44	648	8	596.92	0.0037	0.0	0.0	0.00	0.00	0.00	
			594.53		0.0	0.0	0.00		0.47	

LINE T AT DEVONSHIRE & GILBERT

*** BUENAVISTA DIVERSION Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
45	311	8	598.79	0.0042	0.0	0.0	0.00	0.00	0.00		
			597.49		0.0	0.0	0.00		0.50		
46	337	8	597.49	0.0034	0.0	0.0	0.00	0.00	0.00		
			596.35		0.0	0.0	0.00		0.45		
47	330	8	596.35	0.0055	0.0	0.0	1.06	0.02	3.38		
			594.53		0.0	0.0	0.15		0.58		
48	680	8	594.53	0.0063	0.0	0.0	1.35	0.04	6.70		
			590.22		0.0	0.0	0.21		0.62		
	Lateral length= 1658						Upstream length=		2306		

*** FLORIDA SOUTH LATERAL Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
49	247	6	594.94	0.0100	0.0	0.0	0.80	0.00	0.94		
			592.48		0.0	0.0	0.09		0.36		
50	334	6	592.51	0.0022	0.0	0.0	0.66	0.01	6.98		
			591.78		0.0	0.0	0.21		0.17		
51	329	8	591.76	0.0047	0.0	0.0	1.01	0.02	3.98		
			590.22		0.0	0.0	0.17		0.53		
52	328	8	590.02	0.0088	0.1	0.0	1.77	0.07	9.87		
			587.13		0.0	0.0	0.25		0.73		
53	6	8	587.04	-0.0050	0.1	0.0	0.00	0.08	999.99	0.00	0
			587.07		0.0	0.0	0.00		0.00		0
54	324	8	587.01	0.0038	0.1	0.0	1.31	0.08	16.95		
			585.79		0.0	0.0	0.31		0.48		
55	315	8	585.79	0.0040	0.1	0.0	1.38	0.09	18.27		
			584.53		0.0	0.0	0.33		0.49		
56	70	8	584.53	0.0040	0.1	0.0	1.42	0.10	20.09		
			584.25		0.0	0.0	0.34		0.49		
	Lateral length= 1952						Upstream length=		4258		

LINE T AT DEVONSHIRE & GILBERT

*** FLORIDA NORTH LATERAL
Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
57	12	8	605.76	0.0701	0.1	0.0	4.47	0.13	6.54		
			604.94		0.0	0.0	0.21		2.05		
58	296	8	604.70	0.0071	0.1	0.0	1.90	0.13	20.57		
			602.60		0.0	0.0	0.35		0.65		
59	339	8	602.60	0.0102	0.1	0.0	2.16	0.13	17.19		
			599.16		0.0	0.0	0.32		0.78		
60	318	8	599.16	0.0146	0.1	0.0	2.47	0.13	14.32		
			594.51		0.0	0.0	0.29		0.94		
61	333	8	594.51	0.0046	0.2	0.0	1.87	0.21	39.55		
			592.98		0.0	0.0	0.50		0.52		
62	335	8	592.98	0.0046	0.2	0.0	1.87	0.21	39.52		
			591.44		0.0	0.0	0.50		0.53		
63	322	8	591.44	0.0062	0.2	0.0	2.07	0.21	34.16		
			589.46		0.0	0.0	0.46		0.61		
64	335	8	589.46	0.0071	0.2	0.0	2.17	0.21	31.89		
			587.10		0.0	0.0	0.44		0.65		
65	326	10	587.10	0.0034	0.2	0.0	1.64	0.21	25.29		
			585.99		0.0	0.0	0.39		0.82		
66	311	10	585.99	0.0027	0.2	0.0	1.52	0.21	28.18		
			585.14		0.0	0.0	0.41		0.73		
67	100	10	585.14	0.0089	0.2	0.0	2.28	0.21	15.61		
			584.25		0.0	0.0	0.30		1.33		
68	300	10	584.25	0.0053	0.3	0.0	2.14	0.31	29.94		
			582.67		0.0	0.0	0.43		1.02		
69	335	10	582.67	0.0047	0.3	0.0	2.07	0.31	31.88		
			581.08		0.0	0.0	0.44		0.97		
70	340	10	587.70	0.0241	0.3	0.0	3.69	0.32	14.50		
			579.50		0.0	0.0	0.29		2.18		

Lateral length= 4002 Upstream length= 8260

LINE T AT DEVONSHIRE & GILBERT

*** MAYBERRY LATERAL Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
71	330	8	610.11	0.0025	0.1	0.0	1.20	0.10	24.63		
			609.28		0.0	0.0	0.38		0.39		
72	165	8	609.22	0.0016	0.2	0.0	1.26	0.19	62.16		
			608.96		0.0	0.0	0.64		0.31		
73	165	8	608.99	0.0030	0.2	0.0	1.60	0.21	48.66		
			608.50		0.0	0.0	0.56		0.42		
74	330	8	608.42	0.0091	0.2	0.0	2.44	0.22	30.21		
			605.41		0.0	0.0	0.43		0.74		
75	330	8	605.31	0.0222	0.2	0.0	3.30	0.22	19.38		
			598.00		0.0	0.0	0.34		1.15		
76	332	8	597.97	0.0037	0.3	0.0	1.97	0.31	66.05		
			596.73		0.0	0.0	0.67		0.47		
77	328	8	596.67	0.0029	0.3	0.0	1.83	0.33	77.77		
			595.71		0.0	0.0	0.75		0.42		
78	328	8	595.73	0.0087	0.3	0.0	2.70	0.33	46.45		
			592.89		0.0	0.0	0.54		0.72		
79	331	8	592.87	0.0172	0.3	0.0	3.43	0.33	32.89		
			587.16		0.0	0.0	0.45		1.02		
80	330	8	587.23	-0.0004	0.3	0.0	0.00	0.33	999.99	0.00	0
			587.37		0.0	0.0	0.00		0.00		0
81	332	8	587.36	0.0002	0.3	0.0	0.48	0.35	334.05	0.24	18
			587.30		0.0	0.0	0.90		0.10		18
82	332	8	587.30	0.0117	0.3	0.0	3.03	0.35	41.55		
			583.43		0.0	0.0	0.51		0.84		
83	334	12	583.41	-0.0010	0.4	0.0	0.00	0.36	999.99	0.00	0
			583.73		0.0	0.0	0.00		0.00		0
84	324	12	583.70	0.0074	0.4	0.0	2.45	0.36	18.16		
			581.31		0.0	0.0	0.32		1.96		

Lateral length= 4291 Upstream length= 4294

LINE T AT DEVONSHIRE & GILBERT

*** GILBERT TRUNK — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
85	330	12	581.26	0.0501	0.4	0.0	5.03	0.36	6.96		
			564.73		0.0	0.0	0.21		5.11		
86	334	12	564.73	-0.0040	0.4	0.0	0.00	0.37	999.99	0.00	0
			566.05		0.0	0.0	0.00		0.00		0
87	15	12	580.38	0.0007	0.5	0.0	1.19	0.53	89.98		
			580.37		0.0	0.0	0.82		0.59		
88	324	12	580.37	0.0025	0.5	0.0	1.90	0.53	45.90		
			579.55		0.0	0.0	0.54		1.15		
89	336	12	579.49	0.0015	0.5	0.0	1.57	0.53	60.38		
			579.00		0.0	0.0	0.63		0.87		
90	322	12	578.79	0.0019	0.7	0.0	1.86	0.67	67.84		
			578.18		0.0	0.0	0.68		0.99		
91	325	12	578.14	0.0018	0.7	0.0	1.81	0.67	70.42		
			577.57		0.0	0.0	0.70		0.96		
92	388	12	577.61	0.0022	0.7	0.0	2.01	0.74	70.10		
			576.77		0.0	0.0	0.70		1.06		
93	261	12	576.63	-0.0110	0.7	0.0	0.00	0.74	999.99	0.00	0
			579.50		0.0	0.0	0.00		0.00		0
94	51	12	579.50	0.0709	1.1	0.0	7.50	1.06	17.42		
			575.87		0.0	0.0	0.32		6.08		
95	171	12	575.90	0.0012	1.1	0.0	1.62	1.06	135.45	0.28	10
			575.70		0.0	0.0	0.90		0.78		18
96	270	14	575.70	0.0026	1.1	0.0	2.34	1.06	59.93		
			574.99		0.0	0.0	0.63		1.77		
97	173	14	575.08	0.0036	1.1	0.0	2.60	1.06	51.21		
			574.46		0.0	0.0	0.57		2.07		
98	331	14	574.46	0.0020	1.1	0.0	2.16	1.12	72.98		
			573.80		0.0	0.0	0.72		1.54		
99	339	14	573.80	-0.0016	1.1	0.0	0.00	1.12	999.99	0.00	0
			574.35		0.0	0.0	0.00		0.00		0

LINE T AT DEVONSHIRE & GILBERT

*** GILBERT TRUNK — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
100	19	15	573.35	0.0691	1.5	0.0	8.07	1.49	13.69		
			572.03		0.0	0.0	0.28		10.89		
	Lateral length=		3989		Upstream length=				25318		

```
382: PIP 330.0 619.86  617.26 610.11 609.28 -8!T-230 TO 231
383:
384: REC GHOST2
385:
386: PIP 164.91 617.26 615.63 609.22 608.96 -8!T-231 TO 232
387:
388: SAN 3.0  32.6
389:
390: PIP 164.96 615.63 613.82 608.99 608.50 -8!T-232 TO 235
391:
392: SAN 1.8  32.6
393:
394: SAN 4.9  13.4
395:
396: PIP 329.88 613.82 610.46 608.42 605.41 -8!T-235 TO 236
397:
398: PIP 329.66 610.46 607.29  605.31 598.00 -8!T-236 TO 237
399:
400: REC GHOST3
401:
402: PIP 332.09 607.29 604.03 597.97 596.73 -8!T-237 TO 239
403:
404: SAN 6.7 13.4
405: PIP 328.34 604.03 600.66 596.67 595.71 -8!T-239 TO 242
406: SAN 4.8  13.4
407:
408: PIP 327.91 600.66 597.96 595.73 592.89 -8! T-242 TO 244
409:
410: PIP 331.32  597.96  595.28  592.87  587.16  -8! T-244 TO 247
411:
412: PIP 330.24  595.28  595.26  587.23  587.37  -8!T-247 TO 248
413: SAN 7.1  13.4
414:
415: PIP 331.64  595.26  593.74  587.36  587.30  -8!T-248 TO 251
416: PIP 331.6  593.74  588.69  587.30  583.43  -8!T-251 TO 252
417:
418: SAN 4.5  13.4
419:
420: PIP 334.2  588.69 588.38  583.41  583.73  -12!252 TO 254
421: PIP 324.2  588.38  584.41  583.7 581.31 -12!254 TO 256
422:
423: REM END MAYBERRY - BEGIN GILBERT
424: HOL MAYBERRY
425:
426:
427: NEW GILBERT TRUNK
428:
429: REC MAYBERRY
430: PIP 330.0  584.41 572.64  581.26 564.73  -12!256 TO 257
431:
432:
433: SAN 4.0 13.4  3.6
434:
```

```
435: SAN 4.0  13.4
436:
437: PIP 334.0  572.8  584.99 564.73 566.05 -12!257 TO 188
438: SAN 3.4  13.4
439:
440: REC CENTRAL
441: PIP 15.2  585.1  584.99  580.38  580.37 -12!188 TO 187
442: PIP 324.4  584.99  584.99  580.37  579.55  -12!187 TO 186
443: PIP 336.0  584.99  584.23  579.49  579.0  -12!186 TO 184
444:
445: REC ACACIA
446: PIP 322.2  584.23  585.06  578.79  578.18  -12!184 TO 185
447:
448: PIP 324.9 585.06 586.06 578.14 577.57 -12!185 TO 125
449:
450:
451: SAN 4.3  32.6  9.4
452:
453: SAN 4.4  14  7.4
454:
455: SAN 4.6  32.6 5.6
456:
457: SAN 6.3  24.3
458:
459: PIP 388.3  586.06  587.69  577.61  576.77 -12!125 TO 124
460:
461: PIP 261  587.69  587.7  576.63  579.50  -12!124 TO 118
462: REC FLORIDA_NORTH
463: PIP 51.2 587.7 586.82 579.50 575.87 -12!118 TO 117
464:
465: PIP 170.50 586.82 585.92 575.90 575.70 -12!117 TO 116
466:
467:
468: PIP 270.10  585.92  584.22  575.70  574.99 -14!116 TO 26
469:
470: PIP 172.6  584.22  582.89  575.08  574.46  -14!26 TO 12
471:
472: REM ADD LATHAM LATERAL GHOST SYSTEM,USE DIURNAL CURVE FOR M.H.4
473:
474: DIU 7.16  4.99  3.59  2.14  2.69  9.89  11.55  14.98 +
475:          18.94  19.98  21.62  22.69  19.99  19.48  18.82  19.27+
476:          20.22  18.15  19.04  16.87  13.98  13.13  10.62  8.43
477:
478: SAN 4.2  14  13.1
479:
480: SAN 3.5  14  11.1
481:
482: SAN 6.0  14  9.2
483:
484: SAN 2.0  14  5.6
485:
486: SAN 1.8  32.6  5.6
487:
```

```
488: SAN 4.2  32.6  3.7  ! M.H.4
489:
490: SAN 1.0 32.6  1.8
491:
492: SAN 5.0  14
493:
494: PIP 330.7  582.89  581.23  574.46  573.80  -14!T-12 TO T-11
495:
496: PIP 339  581.23  581.67  573.80  574.35  -14!T-11 TO T-1
497: REC DEVONSHIRE
498:
499: PIP 19.1  581.67  579.43  573.35  572.03  -15  ! T-1  TO T
500:
501: END
```

C:\HYDRA\HEMET\LINE-T.CMD
9:24 22-May-90

------ S U M M A R Y O F A N A L Y S I S ------

Run number on command file	:	1
Number of links	:	100
Number of hydrographs	:	245
Total sanitary population	:	10990
Total sanitary area	:	573.40 Acres
Total storm area	:	0.00 Acres
Number of pumps	:	0
Number of reservoirs	:	0
Number of diversion structures	:	3
Number of inlets	:	0
Length of new pipe	:	0.00 Feet
Length of existing pipe	:	25988.08 Feet
Length of channel	:	0.00 Feet
Length of gutter	:	0.00 Feet
Length of transport units	:	0.00 Feet
Length of pressure pipe	:	0.00 Feet

C:\HYDRA\HEMET\LINE-T20.CMD 17:04 22-May

Status of DEFAULTS at start of run. (* May be reset by SET)

Command file	C:\HYDRA\HEMET\LINE-T20.CMD
Input units are read as	USA
* Output sent to display	Brief
* Output sent to printer	Brief
* Output sent to file	Off
Paper width in inches	8.000
String to reset printer	27 38 108 54 68 27 40 115 49 48 72
String to set printer to compressed	17.16 27 38 107 48 56 72
String to set printer to 8 lines/inch	8 27 38 108 56 68
Name of printer	Hewlett-Packard, LaserJet/LaserJet P
Print heading at top of page	True
Number of steps in hydrograph	96
Step length in minutes	15
Significant flow in hydrograph	0.010
* Maximum plot value	Selected by HYDRA
Type of hydrographic plot	Compact
Sanitary flow by	Diurnal Curve
Delay to start of actual storm	0.00
Rational Method computations	Off
SCS computations	Santa Barbara
Continuous simulation computations	On
* Maximum d/D for pipe design/analysis	0.900
* Match point position on pipe	0.00 or Invert
* Number of allowable diam drops	999
* Mimimum drop thru manhole	0.000
Routing technique	Quick
* Calculate sanitary flows	True
* Calculate infiltration flows	True
* Calculate storm flows	True
* Calculate misc flows	True

```
 1: JOB LINE T AT DEVONSHIRE & GILBERT
 2:
 3: REM --- PIPE AND PIPE COST DATA ---
 4: PDA .013 8 8 7.5 3 .004
 5: CST 1.5 1 3 / .2 .5 .5 2.87 / .5 0 1.63 +
 6:             1.15 / .89 1.1 1.43 4.78
 7: EXC 0/.45  18/.45 30/1.12
 8: TSL 0/0 6/0 6.001/.5 30/.5
 9: PCO 8/2.78  10/4.10  18/9.16  36/18.23
10:
11: REM --- SANITARY CRITERIA ---
12: GPC 100
13:
```

```
:\HYDRA\HEMET\LINE-T20.CMD                                    17:04 22-May-90

14: REM THIS MODEL RUN IS FOR 2010 CONDITIONS
15: REM THE FOLLOWING ARE GHOST SYSTEMS UPSTREAM OF MAYBERRY
16: REM USE MH 5 DIURNAL CURVE
17: DIU 53.67 46.85 44.76 48.62 65.47 108.26 159.47 172.14 +
18:         167.55 166.67 156.81 134.83 138.13 141.07 118.64 131.29 +

19:         139.26 156.17 155.95 143.65 127.75 104.19 87.91 67.28

20:
21: NEW GHOST1  ! MAYBERRY & SANTA FE
22: SAN 8.3  15.4  2.5
23: SAN 6.6  33.0 4.4
24: SAN 3.1  15.4  1.7
25: SAN 11.6  31.1  6.1
26: PIP 1.0  100  100  150  150  -8  ! DUMMY PIPE
27: HOL GHOST1
28:
29: NEW GHOST2  ! MAYBERRY & TAYLOR
30: SAN 7.9  15.4
31: SAN 14.9  37.4  13.3
32: SAN 6.0  15.4 9.4
33: PIP 1.0  100  100  150  150  -8  ! DUMMNY PIPE
34:
35: HOL GHOST2
36:
37: NEW GHOST3   ! MAYBERRY & BUENA VISTA
38: SAN 16.4  15.4  15.8
39: SAN 5.1  15.4 17.5
40: SAN 7.2  15.4  13.3
41: SAN 8.2  15.4  9.2
42: SAN 4.4  15.4  3.1
43: SAN 2.9  15.4  4.7
44: SAN 5.4  15.4  7.5
45: SAN 6.4  7.5  ! CHURCH - ASSUME EQ TO 40 PEOPLE
46: PIP 1.0  100  100  150  150  -8   !  DUMMY PIPE
47: HOL GHOST3
48:
49: NEW GHOST4   ! DEVONSHIRE NEAR HEMET JR HIGH
50: SAN 3.4  37.4  0.0
51: SAN 1.9  37.4  4.6
52: SAN 4.0  37.4  6.4
53: SAN 30.4  16.28  8.3  ! HEMET JR HIGH PER M&E <---
54: SAN 10.1  28.1  11.4
55: PIP 1.0  100  100  150  150  -8  ! DUMMY PIPE
56: HOL GHOST4
57:
58: NEW GHOST5
59: SAN 3.3  14  13.1  ! ALL COMMERCIAL - 100% DEVELOPED
60: SAN 2.7  14  10
61:
62: SAN 13.2  14  16.6
63:
```

```
 64: SAN 5.4  14  3.5
 65:
 66: PIP 1.0  100  100  150  150  -8  !  DUMMNY PIP
 67: HOL GHOST5
 68:
 69: REM BEGIN ANALYSIS  * * * * * * * *
 70:
 71: NEW CALHOUN PLACE
 72:
 73: REM THE FOLLOWING IS ACTUAL DIURNAL CURVE OF M.H. 1
 74:
 75: DIU 21.76  17.93  16.57  17.52  21.63  29.33  36.80  37.28 +
 76:
 77:          56.26  71.05  55.59  43.79  43.08  70.31  67.55  44.92 +
 78:
 79:          36.08  34.03  49.95  63.80  43.19  33.58  30.93  25.53
 80:
 81: SAN 8.2  107.8  8.6  ! P.E. OF 734 BEDS -- SEE CALC'S
 82: SAN 5.5 14 3.6  ! COMM - 100% DEVELOPED
 83:
 84: SAN 3.4  14  ! ZONED R-P
 85: PIP 328.15  603.28  600.50  598.40  596.54  -8  ! T-66 TO t-67
 86: PIP 342.17  600.50  599.25  596.54  591.35  -8  ! T-67 TO T-22
 87:
 88: HOL CALHOUN DRIVE
 89:
 90: NEW BUENA VISTA LATERAL
 91: SAN 2.4  14  1.7
 92:
 93: SAN 5.9  37.4
 94: REC GHOST5
 95: PIP 312.7  599.25  598.9  591.35  590.46  -8  !  T-22 TO T-21
 96: HOL BUENA VISTA
 97:
 98: NEW DEVONSHIRE LATERAL
 99: SAN 1.8  14  8.3
100: REC GHOST4
101: PIP 325.44  601.75  599.49  595.17  591.32  -10  ! T-34 TO T-31
102:
103: SAN 2.6  37.4
104:
105: PIP 167.67  599.49  597.87  591.32  590.46  -10  ! T-31 TO T-21
106:
107: SAN 1.6  37.4
108: REC BUENA VISTA
109: PIP 324.4  597.87  596.34  590.46  589.77  -10  ! T-21 TO T-20
110:
111: SAN 6.1  11.6
112: PIP 338.45  596.34  593.56  589.77  587.75  -10  ! T-20 TO T-19
113:
```

```
114: SAN 5.2  14
115: PIP 321.0  593.56  591.06  587.75  584.89  -10  ! T-19 TO T-17
116:
117: SAN 2.0  14
118:
119: PIP 329.84  591.06  588.09  584.89  581.36  -10  ! T-17 TO T-6
120:
121: SAN 1.7  11.2
122:
123: PIP 53  588.09  588.70  581.36  581.70  -10  ! T-6 TO T-5
124:
125: PIP 325  588.70  588.33  581.70  581.33  -10  ! T-5 TO T-4
126:
127: SAN 4.6  26
128:
129: PIP 334  588.33  586.14  581.33 579.04  -10  ! T-4 TO T-3
130:
131: SAN 4.6  22.8
132:
133: PIP 333  586.14  584.0  579.04  576.70  -10  ! T-3 TO T-2
134:
135: SAN 9.2  35.7
136:
137: PIP 330  584.0  581.67  576.7  574.35  -10  ! T-2 TO T-1
138:
139: HOL DEVONSHIRE
140:
141: NEW CENTRAL LATERAL
142:
143: REM USE M.H.5 DIUNRAL CURVE (R-1)
144:
145: DIU 53.67  46.85 44.76  48.62  65.47  108.26  159.47  172.14 +
146:
147:        167.55 166.67 156.81 134.83 138.13 141.07 118.64 131.29+
148:
149:        139.26  156.17  155.95  143.65  127.75  104.19  87.91  67.28
150: SAN 3.0  37.4  6.7
151:
152: SAN 11.7  29.3
153:
154: DIV OVERFLOW 0 0.67 0/0 0.52/0 1.52/1
155:
156: PIP 331 608.79 605.58 601.29 599.85  -8  ! T-211 TO T-210
157: SAN 3.4  15.4  3.65
158:
159: SAN 2.8  15.4  2.74
160:
161: SAN 2.7  15.4  0.93
162:
163: SAN 1.9  15.4
164:
```

```
165: PIP 162 600.8 599.17 594.52 594.20 -8!T-210,207,204,202,201
166:
167: SAN 1.9  15.4  3.2
168:
169: SAN 4.4  37.4  1.83
170:
171: SAN 2.4  14  1.83
172:
173: PIP 169.2 599.17  598.47  594.2 593.34  -8  ! T-201 TO 198
174:
175: PIP 332.7  598.47  595.19  593.32 589.26 -8!T-198,197,194
176:
177: PIP 326.9  595.19  592.15 589.24 586.22 -8!T-194 TO 191
178:
179: SAN 3.4  15.4
180:
181: PIP 326.7  592.15  589.11 586.28  583.21 -8!191 TO 189
182:
183: SAN 6.3  37.4
184:
185: PIP 329  589.11 585.1 583.23 580.32 -10!189 TO 188
186:
187: HOL CENTRAL
188:
189: NEW MAYBERRY DIVERSION
190:
191:
192: REC OVERFLOW
193:
194: PIP 311.48 608.79 607.30 601.29 600.31 -8!T-211 TO 212
195: PIP 361.75 607.3 605.35  600.31 598.79 -8!T-212 TO 168
196:
197: HOL MAYBERRY_DIV
198:
199: NEW ACACIA LATERAL
200:
201: REM SAME DIURNAL CURVE M.H.5
202:
203: SAN 3.7  30.9  5.56
204:
205: SAN 1.7  33.5  5.56
206:
207: SAN 1.7  33.5  3.72
208:
209: SAN 1.7  33.5  3.72
210:
211: SAN 1.7  33.5  1.78
212:
213: SAN 1.7  29.1  1.78
214:
215: SAN 3.4  15.4
216:
```

```
217: REC MAYBERRY_DIV
218:
219:
220: DIV BUENAVISTA 0 0.67 0/0 0.59/0 1.59/1
221:
222:
223: PIP 330 605.35 603.23 598.79 596.92 -8!T-168 TO 170
224:
225: SAN 4.6  15.4
226:
227: DIV JUANITA 0 0.67 0/0 0.49/0 1.49/1
228:
229:
230: PIP 334  603.23  600.45  596.92  595.56  -8  ! T-170  TO 200
231:
232: SAN 4.8  15.4
233:
234: PIP 330  600.45  598.26  595.56  593.35  -8  !  T-200 TO 172
235:
236: SAN 4.3  15.4
237:
238: PIP 340  598.26  594.95  593.35  590.97  -8  ! T-172 TO 174
239:
240: PIP 329  594.95 592.75  590.97  588.45  -8  ! T-174 TO 176
241: SAN 4.6 37.4
242: PIP 329 592.75 590.37 588.45 585.25 -8! 176 TO 179
243:
244: SAN 9.2  37.4
245:
246: PIP 349  590.37  586.83  585.25  581.46  -8  ! T-179  TO 181
247:
248: PIP 279 586.83 584.35  581.46  578.86  -8  ! T-181 TO 183
249:
250: PIP 7.8  584.35  584.23  578.86  578.85  -8  ! T-183 TO 184
251: HOL ACACIA
252:
253: NEW JUANITA DIVERSION
254:
255: REC JUANITA
256:
257: PIP 648  603.23  600.43  596.92  594.53  -8  ! T-170 TO T-993
258: HOL JUANITA_DIV
259:
260:
261: NEW BUENAVISTA DIVERSION
262:
263: REC BUENAVISTA
264:
265: PIP 310.55  605.35 604.09  598.79  597.49  -8  ! T-168 TO 991
266: PIP 337.33  604.09  601.72 597.49  596.35 -8  ! T-991 TO 992
267: SAN 4.1  37.4
268:
```

```
269: PIP 330  601.72  600.43  596.35  594.53  -8  ! T-992 TO 993
270:
271: SAN 4.6  37.4
272:
273: REC JUANITA_DIV
274:
275: PIP 680 600.43 595.52 594.53 590.22 -8!T-993,994 TO T-94<---
276: HOL BUENAVIS_DIV
277:
278: NEW FLORIDA SOUTH LATERAL
279:
280: SAN 2.0  13.3
281:
282: PIP 247  601.98  598.88  594.94 592.48  -6! T-501 TO T-82
283:
284: SAN 4.1 14
285:
286: PIP 334.2  598.88  597.56  592.51  591.78  -6  ! T-82 TO T-89
287:
288:
289: SAN 4.6 14
290:
291: PIP 328.5  597.56  595.52  591.76  590.22  -8  ! T-89 TO T-94
292:
293:
294: SAN 4.6  14
295:
296: REC BUENAVIS_DIV
297:
298: PIP 327.5  595.52  594.13  590.02  587.13  -8  ! T-94 TO T-100
299:
300: SAN 4.3  14
301:
302: PIP 6.0  594.13  594.10  587.04 587.07  -8  ! T-100 TO T-103
303: PIP 324  594.10 592.72  587.01  585.79  -8  ! T-103 TO T-101
304:
305: SAN 4.4  14
306:
307: PIP 315 592.72 591.5 585.79 584.53 -8!T-101 TO 107*(ASSUMED)<---
308:
309:
310: SAN 4.4  14
311:
312: PIP 70 591.5 591.2 584.53 584.25 -8!T-107 TO 106*(ASSUMED)<---
313: HOL FLORIDA_SOUTH
314:
315: NEW FLORIDA NORTH LATERAL
316:
317: REM CONTINUE R-1 DIURNAL CURVE (M.H.5)
318:
319: SAN 5.8  15.4  12.1
320:
```

```
321: SAN 5.3  15.4  17.7
322:
323: SAN 5.2 15.4 10.0
324:
325: SAN 7.1 15.4  8.3
326:
327: SAN 24.0  15  6.1  ! ACACIA ELEM. SCH. PER M&E <----
328:
329: SAN 7.7 14  1.8
330:
331: SAN 5.2  14  3.6
332:
333: SAN 4.8  14
334:
335: PIP 11.7  611.16  610.94  605.76  604.94 -8  ! T-87 TO 77
336:
337: PIP 296.30  610.94  608.8  604.7  602.6  -8  !  T-77 TO 78
338:
339: PIP 338.7  608.8  605.9 602.6  599.16  -8  ! T-78 TO 79
340:
341: PIP 317.8  605.9  603.0  599.16  594.51  -8  ! T-79 TO 80
342:
343: SAN 4.4  24.6 3.9
344:
345: SAN 4.8  23.4  1.9
346:
347: SAN 2.0  13.3
348:
349: SAN 2.0  14
350:
351: SAN 2.0  37.4  6.7
352:
353: SAN 13.0 15  5.8  !  HEMET EL. SCH. PER M&E <----
354:
355: PIP 333.3  603.0  600.8  594.51  592.98  -8  ! T-80 TO 81
356:
357: PIP 335.1  600.8  598.0  592.98  591.44  -8  ! T-81 TO 90
358:
359: PIP 321.9 598.0  595.9  591.44  589.46  -8  ! T-90 TO 93
360:
361: PIP 334.7  595.9  594.5  589.46  587.10  -8  ! T-93 TO 99
362:
363: PIP 326  594.5  593.0  587.10  585.99  -10  ! T-99 TO 102
364:
365: PIP 311  593.0  592.0  585.99  585.14  -10  ! T-102  TO 104
366:
367: PIP 100 592.0 591.2 585.14 584.25 -10!T-104 TO 106*<---
368:
369: REC FLORIDA_SOUTH
370:
371: PIP 300 591.2 589.85 584.25 582.67 -10!T-106* TO 112<---
372:
```

```
373: SAN 4.6  5.8
374:
375: PIP 335.0  589.85  588.66 582.67 581.08  -10!T-112 TO 115
376:
377: SAN 6.3 10.4
378:
379: PIP 340.0  588.66  587.7 587.7 579.5 -10!T-115 TO 118
380:
381: HOL FLORIDA_NORTH
382:
383:
384: NEW MAYBERRY LATERAL
385:
386: REM BEGIN AT MAYBERRY & SANTA FE W/GHOST SYSTEMS
387:
388: REC GHOST1
389: PIP 330.0 619.86  617.26 610.11 609.28 -8!T-230 TO 231
390:
391: REC GHOST2
392:
393: PIP 164.91 617.26 615.63 609.22 608.96 -8!T-231 TO 232
394:
395: SAN 3.0  37.4
396:
397: PIP 164.96 615.63 613.82 608.99 608.50 -8!T-232 TO 235
398:
399: SAN 1.8  37.4
400:
401: SAN 4.9  15.4
402:
403: PIP 329.88 613.82 610.46 608.42 605.41 -8!T-235 TO 236
404:
405: PIP 329.66 610.46 607.29  605.31 598.00 -8!T-236 TO 237
406:
407: REC GHOST3
408:
409: PIP 332.09 607.29 604.03 597.97 596.73 -8!T-237 TO 239
410:
411: SAN 6.7 15.4
412: PIP 328.34 604.03 600.66 596.67 595.71 -8!T-239 TO 242
413: SAN 4.8  15.4
414:
415: PIP 327.91 600.66 597.96 595.73 592.89 -8! T-242 TO 244
416:
417: PIP 331.32  597.96  595.28  592.87  587.16  -8! T-244 TO 247
418:
419: PIP 330.24  595.28  595.26  587.23  587.37  -8!T-247 TO 248
420: SAN 7.1  15.4
421:
422: PIP 331.64  595.26  593.74  587.36  587.30  -8!T-248 TO 251
423: PIP 331.6  593.74  588.69  587.30  583.43  -8!T-251 TO 252
424:
```

```
425: SAN 4.5  15.4
426:
427: PIP 334.2  588.69 588.38  583.41  583.73  -12!252 TO 254
428: PIP 324.2  588.38  584.41  583.7 581.31 -12!254 TO 256
429:
430:
431: REM END MAYBERRY - BEGIN GILBERT
432:
433: HOL MAYBERRY
434:
435:
436: NEW GILBERT TRUNK
437:
438:
439: REC MAYBERRY
440: PIP 330.0  584.41 572.64  581.26 564.73  -12!256 TO 257
441: SAN 4.0 15.4  3.6
442:
443: SAN 4.0  15.4
444:
445: PIP 334.0  572.8  584.99 564.73 566.05 -12!257 TO 188
446: SAN 3.4  15.4
447:
 48: REC CENTRAL
 49: PIP 15.2  585.1  584.99  580.38  580.37 -12!188 TO 187
450: PIP 324.4  584.99  584.99  580.37  579.55  -12!187 TO 186
451: PIP 336.0  584.99  584.23  579.49  579.0  -12!186 TO 184
452:
453: REC ACACIA
454: PIP 322.2  584.23  585.06  578.79  578.18  -12!184 TO 185
455:
456: PIP 324.9 585.06 586.06 578.14 577.57 -12!185 TO 125
457:
458:
459: SAN 4.3  37.4  9.4
460:
461: SAN 4.4  14  7.4
462:
463: SAN 4.6  37.4 5.6
464:
465: SAN 6.3  27.9
466:
467: PIP 388.3  586.06  587.69  577.61  576.77 -12!125 TO 124
468:
469: PIP 261  587.69  587.7  576.63  579.50  -12!124 TO 118
470: REC FLORIDA_NORTH
471: PIP 51.2 587.7 586.82 579.50 575.87 -12!118 TO 117
472:
473: PIP 170.50 586.82 585.92 575.90 575.70 -12!117 TO 116
 74:
 75:
476: PIP 270.10  585.92  584.22  575.70  574.99 -14!116 TO 26
477:
```

C:\HYDRA\HEMET\LINE-T20.CMD 17:07 22-May-

```
478: PIP 172.6  584.22  582.89  575.08  574.46  -14!26 TO 12
479:
480: REM ADD LATHAM LATERAL GHOST SYSTEM,USE DIURNAL CURVE FOR M.H.4
481:
482:
483: DIU 7.16  4.99  3.59  2.14  2.69  9.89  11.55  14.98 +
484:          18.94  19.98  21.62  22.69  19.99  19.48  18.82  19.27+
485:          20.22  18.15  19.04  16.87  13.98  13.13  10.62  8.43
486:
487: SAN 4.2  14  13.1
488:
489: SAN 3.5  14  11.1
490:
491: SAN 6.0  14  9.2
492:
493: SAN 2.0  14  5.6
494:
495: SAN 1.8  37.4  5.6
496:
497: SAN 4.2  37.4  3.7  ! M.H.4
498:
499: SAN 1.0 37.4  1.8
500:
501: SAN 5.0  14
502:
503: PIP 330.7  582.89  581.23  574.46  573.80  -14!T-12 TO T-11
504:
505: PIP 339  581.23  581.67  573.80  573.35  -14!T-11 TO T-1
506: REC DEVONSHIRE
507:
508: PIP 19.1  581.67  579.43  573.35  572.03  -15  ! T-1  TO T
509:
510: END
```

------ S U M M A R Y O F A N A L Y S I S ------

Run number on command file :	1	
Number of links :	100	
Number of hydrographs :	245	
Total sanitary population :	12540	
Total sanitary area :	573.40	Acres
Total storm area :	0.00	Acres
Number of pumps :	0	
Number of reservoirs :	0	
Number of diversion structures :	3	
Number of inlets :	0	
Length of new pipe :	0.00	Feet
Length of existing pipe :	25988.08	Feet
Length of channel :	0.00	Feet
Length of gutter :	0.00	Feet
Length of transport units :	0.00	Feet
Length of pressure pipe :	0.00	Feet

LINE T AT DEVONSHIRE & GILBERT

*** GHOST1 Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
1	1	8	150.00	0.0000	0.1	0.0	0.00	0.11	999.99	0.00	0
			150.00		0.0	0.0	0.00		0.00		0

Lateral length= 1 Upstream length= 1

*** GHOST2 Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
2	1	8	150.00	0.0000	0.1	0.0	0.00	0.11	999.99	0.00	0
			150.00		0.0	0.0	0.00		0.00		0

Lateral length= 1 Upstream length= 1

*** GHOST3 Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
3	1	8	150.00	0.0000	0.1	0.0	0.00	0.12	999.99	0.00	0
			150.00		0.0	0.0	0.00		0.00		0

Lateral length= 1 Upstream length= 1

*** GHOST4 Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
4	1	8	150.00	0.0000	0.2	0.0	0.00	0.16	999.99	0.00	0
			150.00		0.0	0.0	0.00		0.00		0

Lateral length= 1 Upstream length= 1

*** GHOST5 Analysis of Existing Pi

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
5	1	8	150.00	0.0000	0.1	0.0	0.00	0.05	999.99	0.00	0

LINE T AT DEVONSHIRE & GILBERT

Lateral length= 1 Upstream length= 1

*** CALHOUN PLACE Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
6	328	8	598.40	0.0057	0.2	0.0	1.92	0.18	30.44		
			596.54		0.0	0.0	0.43		0.58		
7	342	8	596.54	0.0152	0.2	0.0	2.70	0.18	18.61		
			591.35		0.0	0.0	0.33		0.95		

Lateral length= 670 Upstream length= 670

*** BUENA VISTA LATERAL Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Rep
8	313	8	591.35	0.0028	0.1	0.0	1.24	0.09	22.63		
			590.46		0.0	0.0	0.36		0.41		

Lateral length= 313 Upstream length= 314

*** DEVONSHIRE LATERAL Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
9	325	10	595.17	0.0118	0.2	0.0	2.43	0.17	10.89		
			591.32		0.0	0.0	0.26		1.53		
10	168	10	591.32	0.0051	0.2	0.0	1.80	0.18	17.92		
			590.46		0.0	0.0	0.32		1.01		
11	324	10	590.46	0.0021	0.3	0.0	1.52	0.28	43.85		
			589.77		0.0	0.0	0.52		0.65		
12	338	10	589.77	0.0060	0.3	0.0	2.23	0.30	27.32		
			587.75		0.0	0.0	0.41		1.09		
13	321	10	587.75	0.0089	0.3	0.0	2.58	0.31	23.33		
			584.89		0.0	0.0	0.37		1.33		
14	330	10	584.89	0.0107	0.3	0.0	2.76	0.31	21.62		
			581.36		0.0	0.0	0.36		1.45		

LINE T AT DEVONSHIRE & GILBERT

*** DEVONSHIRE LATERAL — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
15	53	10	581.36	-0.0064	0.3	0.0	0.00	0.32	999.99	0.00	0
			581.70		0.0	0.0	0.00		0.00		0
16	325	10	581.70	0.0011	0.3	0.0	1.27	0.32	67.01		
			581.33		0.0	0.0	0.68		0.47		
17	334	10	581.33	0.0069	0.3	0.0	2.43	0.34	29.12		
			579.04		0.0	0.0	0.42		1.16		
18	333	10	579.04	0.0070	0.4	0.0	2.48	0.36	30.31		
			576.70		0.0	0.0	0.43		1.18		
19	330	10	576.70	0.0071	0.4	0.0	2.61	0.41	34.97		
			574.35		0.0	0.0	0.46		1.19		

Lateral length= 3182 Upstream length= 3497

*** CENTRAL LATERAL — Diversion

Link	Invert Up/Dn		Maximum Flow Values San	Inf	Sto	Mis	Design	Cost
21	Unknown	Discharge :	0.07	0.00	0.00	0.00	0.07	0
	Unknown	Diverted :	0.00	0.00	0.00	0.00	0.00	
		Incoming :	0.07	0.00	0.00	0.00	0.07	

*** CENTRAL LATERAL — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
22	331	8	601.29	0.0044	0.1	0.0	1.31	0.07	12.97		
			599.85		0.0	0.0	0.28		0.51		
23	162	8	594.52	0.0020	0.1	0.0	1.09	0.09	26.28		
			594.20		0.0	0.0	0.40		0.34		
24	169	8	594.20	0.0051	0.1	0.0	1.66	0.12	22.38		
			593.34		0.0	0.0	0.36		0.55		
25	333	8	593.32	0.0122	0.1	0.0	2.26	0.12	14.44		
			589.26		0.0	0.0	0.29		0.86		

LINE T AT DEVONSHIRE & GILBERT

*** CENTRAL LATERAL — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
26	327	8	589.24	0.0092	0.1	0.0	2.04	0.12	16.60		
			586.22		0.0	0.0	0.31		0.74		
27	327	8	586.28	0.0094	0.1	0.0	2.08	0.13	17.47		
			583.21		0.0	0.0	0.32		0.75		
28	329	10	583.23	0.0088	0.2	0.0	2.16	0.17	12.53		
			580.32		0.0	0.0	0.28		1.32		
	Lateral length= 1978				Upstream length= 1978						

*** MAYBERRY DIVERSION — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Rep
29	311	8	601.29	0.0031	0.0	0.0	0.00	0.00	0.00		
			600.31		0.0	0.0	0.00		0.43		
30	362	8	600.31	0.0042	0.0	0.0	0.00	0.00	0.00		
			598.79		0.0	0.0	0.00		0.50		
	Lateral length= 673				Upstream length= 673						

*** ACACIA LATERAL — Diversion

Link	Invert Up/Dn	Maximum Flow Values	San	Inf	Sto	Mis	Design	Cost
32	598.79	Discharge :	0.06	0.00	0.00	0.00	0.06	0
	598.79	Diverted :	0.00	0.00	0.00	0.00	0.00	
		Incoming :	0.06	0.00	0.00	0.00	0.06	

*** ACACIA LATERAL — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
33	330	8	598.79	0.0057	0.1	0.0	1.45	0.06	11.09		
			596.92		0.0	0.0	0.26		0.58		

LINE T AT DEVONSHIRE & GILBERT

*** ACACIA LATERAL Diversion

Link	Invert Up/Dn		Maximum Flow Values San	Inf	Sto	Mis	Design	Cost
35	596.92	Discharge :	0.07	0.00	0.00	0.00	0.07	0
	596.92	Diverted :	0.00	0.00	0.00	0.00	0.00	
		Incoming :	0.07	0.00	0.00	0.00	0.07	

*** ACACIA LATERAL Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
36	334	8	596.92	0.0041	0.1	0.0	1.32	0.07	15.17		
			595.56		0.0	0.0	0.30		0.49		
37	330	8	595.56	0.0067	0.1	0.0	1.65	0.09	13.52		
			593.35		0.0	0.0	0.28		0.63		
38	340	8	593.35	0.0070	0.1	0.0	1.72	0.10	14.72		
			590.97		0.0	0.0	0.29		0.65		
39	329	8	590.97	0.0077	0.1	0.0	1.78	0.10	14.07		
			588.45		0.0	0.0	0.29		0.68		
40	329	8	588.45	0.0097	0.1	0.0	2.06	0.12	15.76		
			585.25		0.0	0.0	0.30		0.76		
41	349	8	585.25	0.0109	0.2	0.0	2.37	0.17	21.11		
			581.46		0.0	0.0	0.35		0.81		
42	279	8	581.46	0.0093	0.2	0.0	2.26	0.17	22.78		
			578.86		0.0	0.0	0.37		0.75		
43	8	8	578.86	0.0013	0.2	0.0	1.13	0.17	61.38		
			578.85		0.0	0.0	0.64		0.28		

Lateral length= 2628 Upstream length= 3301

*** JUANITA DIVERSION Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
44	648	8	596.92	0.0037	0.0	0.0	0.00	0.00	0.00		
			594.53		0.0	0.0	0.00		0.47		

Lateral length= 648 Upstream length= 648

```
223: SAN 4.6  13.4
224:
225: DIV JUANITA 0 0.67 0/0 0.49/0 1.49/1
226:
227:
228: PIP 334  603.23  600.45  596.92  595.56  -8  ! T-170  TO 200
229:
230: SAN 4.8  13.4
231:
232: PIP 330  600.45  598.26  595.56  593.35  -8  !  T-200 TO 172
233:
234: SAN 4.3  13.4
235:
236: PIP 340  598.26  594.95  593.35  590.97  -8  ! T-172 TO 174
237:
238: PIP 329  594.95 592.75  590.97  588.45  -8  ! T-174 TO 176
239: SAN 4.6 32.6
240: PIP 329 592.75 590.37 588.45 585.25 -8! 176 TO 179
241:
242: SAN 9.2  32.6
243:
244: PIP 349  590.37  586.83  585.25  581.46  -8  ! T-179  TO 181
245:
246: PIP 279 586.83 584.35  581.46  578.86  -8  ! T-181 TO 183
247:
248: PIP 7.8  584.35  584.23  578.86  578.85  -8  ! T-183 TO 184
249: HOL ACACIA
250:
251: NEW JUANITA DIVERSION
252:
253: REC JUANITA
254:
255: PIP 648  603.23  600.43  596.92  594.53  -8  ! T-170 TO T-993
256: HOL JUANITA_DIV
257:
258:
259: NEW BUENAVISTA DIVERSION
260:
261: REC BUENAVISTA
262:
263: PIP 310.55  605.35 604.09  598.79  597.49  -8  ! T-168 TO 991
264: PIP 337.33  604.09  601.72 597.49  596.35 -8  ! T-991 TO 992
265: SAN 4.1  32.6
266:
267: PIP 330  601.72  600.43  596.35  594.53  -8  ! T-992 TO 993
268:
269: SAN 4.6  32.6
270:
271: REC JUANITA_DIV
272:
273: PIP 680 600.43 595.52 594.53 590.22 -8!T-993,994 TO T-94<---
274: HOL BUENAVIS_DIV
275:
```

```
276: NEW FLORIDA SOUTH LATERAL
277:
278: SAN 2.0  11.6
279:
280: PIP 247  601.98  598.88  594.94 592.48  -6! T-501 TO T-82
281:
282: SAN 4.1 14
283:
284: PIP 334.2  598.88  597.56  592.51  591.78  -6  ! T-82 TO T-89
285: SAN 4.6 14
286: PIP 328.5  597.56  595.52  591.76  590.22  -8  ! T-89 TO T-94
287:
288: SAN 4.6  14
289: REC BUENAVIS_DIV
290:
291: PIP 327.5  595.52  594.13  590.02  587.13  -8  ! T-94 TO T-100
292:
293: SAN 4.3  14
294:
295: PIP 6.0  594.13  594.10  587.04 587.07  -8  ! T-100 TO T-103
296: PIP 324  594.10 592.72  587.01  585.79  -8  ! T-103 TO T-101
297:
298: SAN 4.4  14
299:
300: PIP 315 592.72 591.5 585.79 584.53 -8!T-101 TO 107*(ASSUMED)<---
301:
302: SAN 4.4  14
303:
304: PIP 70 591.5 591.2 584.53 584.25 -8!T-107 TO 106*(ASSUMED)<---
305: HOL FLORIDA_SOUTH
306:
307: NEW FLORIDA NORTH LATERAL
308:
309: REM CONTINUE R-1 DIURNAL CURVE (M.H.5)
310:
311: SAN 5.8  13.4  12.1
312:
313: SAN 5.3  13.4  17.7
314:
315: SAN 5.2 13.4 10.0
316:
317: SAN 7.1 13.4  8.3
318:
319: SAN 24.0  15  6.1  ! ACACIA ELEM. SCH. PER M&E <----
320:
321: SAN 7.7 14  1.8
322:
323: SAN 5.2  14  3.6
324:
325: SAN 4.8  14
326:
327: PIP 11.7  611.16  610.94  605.76  604.94 -8  ! T-87 TO 77
328:
```

```
329: PIP 296.30  610.94  608.8  604.7  602.6  -8  ! T-77 TO 78
330:
331: PIP 338.7  608.8  605.9 602.6  599.16  -8  ! T-78 TO 79
332:
333: PIP 317.8  605.9  603.0  599.16  594.51  -8  ! T-79 TO 80
334:
335: SAN 4.4  21.5 3.9
336:
337: SAN 4.8  20.4  1.9
338:
339: SAN 2.0  11.6
340:
341: SAN 2.0  14
342:
343: SAN 2.0  32.6  6.7
344:
345: SAN 13.0 15  5.8  !  HEMET EL. SCH. PER M&E <----
346:
347: PIP 333.3  603.0  600.8  594.51  592.98  -8  ! T-80 TO 81
348:
349: PIP 335.1  600.8  598.0  592.98  591.44  -8  ! T-81 TO 90
350:
351: PIP 321.9 598.0  595.9  591.44  589.46  -8  ! T-90 TO 93
352:
353: PIP 334.7  595.9  594.5  589.46  587.10  -8  ! T-93 TO 99
354:
355: PIP 326  594.5  593.0  587.10  585.99  -10  ! T-99 TO 102
356:
357: PIP 311  593.0  592.0  585.99  585.14  -10  ! T-102  TO 104
358:
359: PIP 100 592.0 591.2 585.14 584.25 -10!T-104 TO 106*<---
360:
361: REC FLORIDA_SOUTH
362:
363: PIP 300 591.2 589.85 584.25 582.67 -10!T-106* TO 112<---
364:
365: SAN 4.6  5.1
366:
367: PIP 335.0  589.85  588.66 582.67 581.08  -10!T-112 TO 115
368:
369: SAN 6.3 8.8
370:
371: PIP 340.0  588.66  587.7 587.7 579.5 -10!T-115 TO 118
372:
373: HOL FLORIDA_NORTH
374:
375:
376: NEW MAYBERRY LATERAL
377:
378: REM BEGIN AT MAYBERRY & SANTA FE W/GHOST SYSTEMS
379:
380: REC GHOST1
381:
```

C:\HYDRA\HEMET\LINE-T20.CMD 17:08 22-May-90

LINE T AT DEVONSHIRE & GILBERT

*** BUENAVISTA DIVERSION Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
45	311	8	598.79	0.0042	0.0	0.0	0.00	0.00	0.00		
			597.49		0.0	0.0	0.00		0.50		
46	337	8	597.49	0.0034	0.0	0.0	0.00	0.00	0.00		
			596.35		0.0	0.0	0.00		0.45		
47	330	8	596.35	0.0055	0.0	0.0	1.09	0.02	3.88		
			594.53		0.0	0.0	0.16		0.58		
48	680	8	594.53	0.0063	0.0	0.0	1.40	0.05	7.68		
			590.22		0.0	0.0	0.22		0.62		
	Lateral length= 1658					Upstream length= 2306					

*** FLORIDA SOUTH LATERAL Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
49	247	6	594.94	0.0100	0.0	0.0	0.84	0.00	1.08		
			592.48		0.0	0.0	0.09		0.36		
50	334	6	592.51	0.0022	0.0	0.0	0.67	0.01	7.28		
			591.78		0.0	0.0	0.22		0.17		
51	329	8	591.76	0.0047	0.0	0.0	1.02	0.02	4.07		
			590.22		0.0	0.0	0.17		0.53		
52	328	8	590.02	0.0088	0.1	0.0	1.80	0.08	10.77		
			587.13		0.0	0.0	0.26		0.73		
53	6	8	587.04	-0.0050	0.1	0.0	0.00	0.09	999.99	0.00	0
			587.07		0.0	0.0	0.00		0.00		0
54	324	8	587.01	0.0038	0.1	0.0	1.34	0.09	18.33		
			585.79		0.0	0.0	0.33		0.48		
55	315	8	585.79	0.0040	0.1	0.0	1.41	0.10	19.62		
			584.53		0.0	0.0	0.34		0.49		
56	70	8	584.53	0.0040	0.1	0.0	1.45	0.11	21.43		
			584.25		0.0	0.0	0.35		0.49		
	Lateral length= 1952					Upstream length= 4258					

LINE T AT DEVONSHIRE & GILBERT

*** FLORIDA NORTH LATERAL — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
57	12	8	605.76	0.0701	0.1	0.0	4.53	0.14	6.87		
			604.94		0.0	0.0	0.21		2.05		
58	296	8	604.70	0.0071	0.1	0.0	1.93	0.14	21.62		
			602.60		0.0	0.0	0.36		0.65		
59	339	8	602.60	0.0102	0.1	0.0	2.19	0.14	18.06		
			599.16		0.0	0.0	0.32		0.78		
60	318	8	599.16	0.0146	0.1	0.0	2.50	0.14	15.05		
			594.51		0.0	0.0	0.30		0.94		
61	333	8	594.51	0.0046	0.2	0.0	1.91	0.22	41.98		
			592.98		0.0	0.0	0.51		0.52		
62	335	8	592.98	0.0046	0.2	0.0	1.91	0.22	41.96		
			591.44		0.0	0.0	0.51		0.53		
63	322	8	591.44	0.0062	0.2	0.0	2.11	0.22	36.27		
			589.46		0.0	0.0	0.47		0.61		
64	335	8	589.46	0.0071	0.2	0.0	2.21	0.22	33.85		
			587.10		0.0	0.0	0.45		0.65		
65	326	10	587.10	0.0034	0.2	0.0	1.68	0.22	26.85		
			585.99		0.0	0.0	0.40		0.82		
66	311	10	585.99	0.0027	0.2	0.0	1.54	0.22	29.92		
			585.14		0.0	0.0	0.43		0.73		
67	100	10	585.14	0.0089	0.2	0.0	2.32	0.22	16.58		
			584.25		0.0	0.0	0.31		1.33		
68	300	10	584.25	0.0053	0.3	0.0	2.18	0.32	31.83		
			582.67		0.0	0.0	0.44		1.02		
69	335	10	582.67	0.0047	0.3	0.0	2.11	0.33	33.92		
			581.08		0.0	0.0	0.45		0.97		
70	340	10	587.70	0.0241	0.3	0.0	3.75	0.34	15.47		
			579.50		0.0	0.0	0.30		2.18		

Lateral length= 4002 Upstream length= 8260

LINE T AT DEVONSHIRE & GILBERT

*** MAYBERRY LATERAL

Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
71	330	8	610.11	0.0025	0.1	0.0	1.26	0.11	28.27		
			609.28		0.0	0.0	0.41		0.39		
72	165	8	609.22	0.0016	0.2	0.0	1.32	0.22	72.22		
			608.96		0.0	0.0	0.71		0.31		
73	165	8	608.99	0.0030	0.2	0.0	1.68	0.24	56.48		
			608.50		0.0	0.0	0.61		0.42		
74	330	8	608.42	0.0091	0.3	0.0	2.54	0.26	35.04		
			605.41		0.0	0.0	0.46		0.74		
75	330	8	605.31	0.0222	0.3	0.0	3.46	0.26	22.48		
			598.00		0.0	0.0	0.36		1.15		
76	332	8	597.97	0.0037	0.4	0.0	2.09	0.38	79.75		
			596.73		0.0	0.0	0.76		0.47		
77	328	8	596.67	0.0029	0.4	0.0	1.92	0.39	93.71		
			595.71		0.0	0.0	0.85		0.42		
78	328	8	595.73	0.0087	0.4	0.0	2.86	0.40	55.90		
			592.89		0.0	0.0	0.60		0.72		
79	331	8	592.87	0.0172	0.4	0.0	3.63	0.40	39.59		
			587.16		0.0	0.0	0.50		1.02		
80	330	8	587.23	-0.0004	0.4	0.0	0.00	0.40	999.99	0.00	0
			587.37		0.0	0.0	0.00		0.00		0
81	332	8	587.36	0.0002	0.4	0.0	0.48	0.42	401.35	0.31	18
			587.30		0.0	0.0	0.90		0.10		18
82	332	8	587.30	0.0117	0.4	0.0	3.20	0.42	49.92		
			583.43		0.0	0.0	0.56		0.84		
83	334	12	583.41	-0.0010	0.4	0.0	0.00	0.43	999.99	0.00	0
			583.73		0.0	0.0	0.00		0.00		0
84	324	12	583.70	0.0074	0.4	0.0	2.59	0.43	21.79		
			581.31		0.0	0.0	0.36		1.96		

Lateral length= 4291 Upstream length= 4294

LINE T AT DEVONSHIRE & GILBERT

*** GILBERT TRUNK Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
85	330	12	581.26	0.0501	0.4	0.0	5.29	0.43	8.36		
			564.73		0.0	0.0	0.23		5.11		
86	334	12	564.73	-0.0040	0.4	0.0	0.00	0.44	999.99	0.00	0
			566.05		0.0	0.0	0.00		0.00		0
87	15	12	580.38	0.0007	0.6	0.0	1.21	0.62	105.10	0.03	8
			580.37		0.0	0.0	0.90		0.59		18
88	324	12	580.37	0.0025	0.6	0.0	2.00	0.62	53.61		
			579.55		0.0	0.0	0.59		1.15		
89	336	12	579.49	0.0015	0.6	0.0	1.65	0.62	70.54		
			579.00		0.0	0.0	0.70		0.87		
90	322	12	578.79	0.0019	0.8	0.0	1.94	0.78	78.85		
			578.18		0.0	0.0	0.75		0.99		
91	325	12	578.14	0.0018	0.8	0.0	1.89	0.78	81.85		
			577.57		0.0	0.0	0.77		0.96		
92	388	12	577.61	0.0022	0.9	0.0	2.09	0.86	81.26		
			576.77		0.0	0.0	0.77		1.06		
93	261	12	576.63	-0.0110	0.9	0.0	0.00	0.86	999.99	0.00	0
			579.50		0.0	0.0	0.00		0.00		0
94	51	12	579.50	0.0709	1.2	0.0	7.78	1.20	19.72		
			575.87		0.0	0.0	0.34		6.08		
95	171	12	575.90	0.0012	1.2	0.0	1.62	1.20	153.32	0.42	10
			575.70		0.0	0.0	0.90		0.78		18
96	270	14	575.70	0.0026	1.2	0.0	2.43	1.20	67.83		
			574.99		0.0	0.0	0.68		1.77		
97	173	14	575.08	0.0036	1.2	0.0	2.71	1.20	57.97		
			574.46		0.0	0.0	0.62		2.07		
98	331	14	574.46	0.0020	1.3	0.0	2.24	1.27	82.30		
			573.80		0.0	0.0	0.77		1.54		
99	339	14	573.80	0.0013	1.3	0.0	1.91	1.27	100.92	0.01	8
			573.35		0.0	0.0	0.90		1.26		18

C:\HYDRA\HEMET\LINE-T20.CMD 17:08 22-May-90

LINE T AT DEVONSHIRE & GILBERT

*** GILBERT TRUNK Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
100	19	15	573.35	0.0691	1.7	0.0	8.29	1.66	15.25		
			572.03		0.0	0.0	0.30		10.89		

Lateral length= 3989 Upstream length= 25318

C:\HYDRA\HEMET\LINE-Y.CMD 17:09 22-May-..

Status of DEFAULTS at start of run. (* May be reset by SET)

Command file	C:\HYDRA\HEMET\LINE-Y.CMD
Input units are read as	USA
* Output sent to display	Brief
* Output sent to printer	Brief
* Output sent to file	Off
Paper width in inches	8.000
String to reset printer	27 38 108 54 68 27 40 115 49 48 72
String to set printer to compressed	17.16 27 38 107 48 56 72
String to set printer to 8 lines/inch	8 27 38 108 56 68
Name of printer	Hewlett-Packard, LaserJet/LaserJet I
Print heading at top of page	True
Number of steps in hydrograph	96
Step length in minutes	15
Significant flow in hydrograph	0.010
* Maximum plot value	Selected by HYDRA
Type of hydrographic plot	Compact
Sanitary flow by	Diurnal Curve
Delay to start of actual storm	0.00
Rational Method computations	Off
SCS computations	Santa Barbara
Continuous simulation computations	On
* Maximum d/D for pipe design/analysis	0.900
* Match point position on pipe	0.00 or Invert
* Number of allowable diam drops	999
* Mimimum drop thru manhole	0.000
Routing technique	Quick
* Calculate sanitary flows	True
* Calculate infiltration flows	True
* Calculate storm flows	True
* Calculate misc flows	True

```
 1: JOB LINE Y AT STETSON & PALM
 2:
 3: REM --- PIPE AND PIPE COST DATA ---
 4: PDA .013 8 8 7.5 3 .004
 5: CST 1.5 1 3/ .2 .5 .5 2.87 / .5 0 1.63+
 6:         1.15/ .89 1.1 1.43 4.78
 7: EXC 0/ .45 18/.45 30/1.12
 8: TSL 0/0 6/0 6.001/.5 30/.5
 9: PCO 8/ 2.78 10/4.10 18/9.16 36/18.23
10: REM --- SANITARY CRITERIA ---
11: GPC 100 ! AVERAGE DAILY FLOW PER CAPITA
12: REM THIS MODEL RUN IS FOR 1990 CONDITIONS
13:
```

C:\HYDRA\HEMET\LINE-Y.CMD 17:09 22-May-90

```
 14: REM USE M.H.4 DIURNAL CURVE
 15: DIU 7.16 4.99 3.59 2.14 2.69 9.89 11.55 14.98+
 16:          18.94 19.98 21.62 22.69 19.99 19.48 18.82 19.27+
 17:          20.22 18.15 19.04 16.87 13.98 13.13 10.62 8.43
 18:
 19: NEW THORNTON LATERAL
 20: SAN 10.8 10.8 4.3
 21: SAN 8.5 10.8 5.8
 22: SAN 2.5 14 8.6
 23: SAN 8.7 15.5
 24: SAN 9.2 32.6 1.4
 25: SAN 8.6 10.8 3.1
 26: SAN 18.9 32.6 4.7
 27: SAN 2.5 10.8 8.8
 28: SAN 5.5 14 12.4
 29: SAN 2.8 0.0 12.4
 30: SAN 7.4 10.8 16.0
 31: SAN 2.5 14 16.0
 32: SAN 8.0 19.6 16.0
 33: SAN 4.3 10.8 17.8
 34: SAN 1.5 14 17.8
 35: SAN 4.8 19.6 17.8
 36: SAN 10.0 14 20.1
 37: SAN 4.0 19.6 20.1
 38: PIP 335 570.56 567.52 560.07 559.03 -10! Y42 TO Y12
 39: PIP 225 567.52 566.03 559.03 558.44 -10! 12 TO 11
 40: SAN 9.2 10.8
 41: SAN 8.1 10.8 1.4
 42: SAN 8.7 10.8 4.3
 43: PIP 100 566.03 565.18 558.44 558.12 -10! 11 TO 10
 44: PIP 321 565.18 563.80 558.12 557.21 -10! 10 TO 9
 45: PIP 335 563.80 562.24 557.21 556.28 -10! 9 TO 8
 46: SAN 8.5 10.8
 47: SAN 11.7 10.8 3.3
 48: SAN 11.7 10.8 6.1
 49: SAN 10.0 0.0 10.3
 50: SAN 8.0 0.0 14.6
 51: SAN 15.2 0.0 19.6
 52: PIP 346 562.24 563.23 556.28 555.50 -10! 8 TO 7
 53: SAN 5.2 10.8 1.8
 54: PIP 90.97 563.23 563.60 555.50 555.21 -10! 7 TO 6
 55: PIP 155.03 563.60 564.0 555.21 554.75 -10! 6 TO 5
 56: SAN 4.0 10.8
 57: PIP 216.06 564.0 564.5 554.75 554.23 -10! 5 TO 4
 58: PIP 68 564.5 564.75 554.23 554.04 -10! 4 TO 3
 59: SAN 4.5 10.8
 60: PIP 200 564.75 564.0 554.04 553.48 -10! 3 TO 2
 61: SAN 4.2 10.8
 62: SAN 5.1 5.1
 63: PIP 224 564.0 567.26 553.48 551.26 -10! Y-2 TO Y-1
  4: END
```

------ S U M M A R Y O F A N A L Y S I S ------

Run number on command file :	1	
Number of links :	12	
Number of hydrographs :	50	
Total sanitary population :	2988	
Total sanitary area :	234.60	Acres
Total storm area :	0.00	Acres
Number of pumps :	0	
Number of reservoirs :	0	
Number of diversion structures :	0	
Number of inlets :	0	
Length of new pipe :	0.00	Feet
Length of existing pipe :	2616.06	Feet
Length of channel :	0.00	Feet
Length of gutter :	0.00	Feet
Length of transport units :	0.00	Feet
Length of pressure pipe :	0.00	Feet

C:\HYDRA\HEMET\LINE-Y.CMD 17:09 22-May-90

LINE Y AT STETSON & PALM

*** THORNTON LATERAL Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
1	335	10	560.07	0.0031	0.3	0.0	1.84	0.35	44.07		
			559.03		0.0	0.0	0.53		0.78		
2	225	10	559.03	0.0026	0.3	0.0	1.74	0.35	47.96		
			558.44		0.0	0.0	0.55		0.72		
3	100	10	558.44	0.0032	0.4	0.0	1.94	0.39	49.10		
			558.12		0.0	0.0	0.56		0.79		
4	321	10	558.12	0.0028	0.4	0.0	1.86	0.39	52.17		
			557.21		0.0	0.0	0.58		0.75		
5	335	10	557.21	0.0028	0.4	0.0	1.84	0.39	52.72		
			556.28		0.0	0.0	0.58		0.74		
6	346	10	556.28	0.0023	0.4	0.0	1.79	0.45	66.81		
			555.50		0.0	0.0	0.68		0.67		
7	91	10	555.50	0.0032	0.5	0.0	2.03	0.45	57.28		
			555.21		0.0	0.0	0.61		0.79		
8	155	10	555.21	0.0030	0.5	0.0	1.98	0.45	59.36		
			554.75		0.0	0.0	0.63		0.77		
9	216	10	554.75	0.0024	0.5	0.0	1.85	0.46	66.90		
			554.23		0.0	0.0	0.68		0.69		
10	68	10	554.23	0.0028	0.5	0.0	1.95	0.46	62.05		
			554.04		0.0	0.0	0.64		0.74		
11	200	10	554.04	0.0028	0.5	0.0	1.96	0.47	63.03		
			553.48		0.0	0.0	0.65		0.74		
12	224	10	553.48	0.0099	0.5	0.0	3.06	0.48	34.31		
			551.26		0.0	0.0	0.46		1.40		

Lateral length= 2616 Upstream length= 2616

C:\HYDRA\HEMET\LINE-Y20.CMD 17:10 22-May-90

Status of DEFAULTS at start of run. (* May be reset by SET)

Command file	C:\HYDRA\HEMET\LINE-Y20.CMD
Input units are read as	USA
* Output sent to display	Brief
* Output sent to printer	Brief
* Output sent to file	Off
Paper width in inches	8.000
String to reset printer	27 38 108 54 68 27 40 115 49 48 72
String to set printer to compressed	17.16 27 38 107 48 56 72
String to set printer to 8 lines/inch	8 27 38 108 56 68
Name of printer	Hewlett-Packard, LaserJet/LaserJet I
Print heading at top of page	True
Number of steps in hydrograph	96
Step length in minutes	15
Significant flow in hydrograph	0.010
* Maximum plot value	Selected by HYDRA
Type of hydrographic plot	Compact
Sanitary flow by	Diurnal Curve
Delay to start of actual storm	0.00
Rational Method computations	Off
SCS computations	Santa Barbara
Continuous simulation computations	On
* Maximum d/D for pipe design/analysis	0.900
* Match point position on pipe	0.00 or Invert
* Number of allowable diam drops	999
* Mimimum drop thru manhole	0.000
Routing technique	Quick
* Calculate sanitary flows	True
* Calculate infiltration flows	True
* Calculate storm flows	True
* Calculate misc flows	True

```
 1: JOB LINE Y AT STETSON & PALM
 2:
 3: REM --- PIPE AND PIPE COST DATA ---
 4: PDA .013 8 8 7.5 3 .004
 5: CST 1.5 1 3/ .2 .5 .5 2.87 / .5 0 1.63+
 6:         1.15/ .89 1.1 1.43 4.78
 7: EXC 0/ .45 18/.45 30/1.12
 8: TSL 0/0 6/0 6.001/.5 30/.5
 9: PCO 8/ 2.78 10/4.10 18/9.16 36/18.23
10: REM --- SANITARY CRITERIA ---
11: GPC 100 ! AVERAGE DAILY FLOW PER CAPITA
12: REM THIS MODEL RUN IS FOR 2010 CONDITIONS
13:
```

.\HYDRA\HEMET\LINE-Y20.CMD 17:10 22-May-90

```
14: REM USE M.H.4 DIURNAL CURVE
15: DIU 7.16 4.99 3.59 2.14 2.69 9.89 11.55 14.98+
16:         18.94 19.98 21.62 22.69 19.99 19.48 18.82 19.27+
17:         20.22 18.15 19.04 16.87 13.98 13.13 10.62 8.43
18:
19: NEW THORNTON LATERAL
20: SAN 10.8 15.4 4.3
21: SAN 8.5 15.4 5.8
22: SAN 2.5 14 8.6
23: SAN 8.7 20.0
24: SAN 9.2 37.4 1.4
25: SAN 8.6 15.4 3.1
26: SAN 18.9 37.4 4.7
27: SAN 2.5 15.4 8.8
28: SAN 5.5 14 12.4
29: SAN 2.8 19.6 12.4
30: SAN 7.4 15.4 16.0
31: SAN 2.5 14 16.0
32: SAN 8.0 37.4 16.0
33: SAN 4.3 15.4 17.8
34: SAN 1.5 14 17.8
35: SAN 4.8 37.4 17.8
36: SAN 10.0 14 20.1
37: SAN 4.0 37.4 20.1
38: PIP 335 570.56 567.52 560.07 559.03 -10! Y42- TO Y12
39: PIP 225 567.52 566.03 559.03 558.44 -10! 12 TO 11
40: SAN 9.2 15.4
41: SAN 8.1 15.4 1.4
42: SAN 8.7 15.4 4.3
43: PIP 100 566.03 565.18 558.44 558.12 -10! 11 TO 10
44: PIP 321 565.18 563.80 558.12 557.21 -10! 10 TO 9
45: PIP 335 563.80 562.24 557.21 556.28 -10! 9 TO 8
46: SAN 8.5 15.4
47: SAN 11.7 15.4 3.3
48: SAN 11.7 15.4 6.1
49: SAN 10.0 19.6 10.3
50: SAN 8.0 19.6 14.6
51: SAN 15.2 19.6 19.6
52: PIP 346 562.24 563.23 556.28 555.50 -10! 8 TO 7
53: SAN 5.2 15.4 1.8
54: PIP 90.97 563.23 563.60 555.50 555.21 -10! 7 TO 6
55: PIP 155.03 563.60 564.0 555.21 554.75 -10! 6 TO 5
56: SAN 4.0 15.4
57: PIP 216.06 564.0 564.5 554.75 554.23 -10! 5 TO 4
58: PIP 68 564.5 564.75 554.23 554.04 -10! 4 TO 3
59: SAN 4.5 15.4
60: PIP 200 564.75 564.0 554.04 553.48 -10! 3 TO 2
61: SAN 4.2 15.4
62: SAN 5.1 32.8
63: PIP 224 564.0 567.26 553.48 551.26 -10! Y-2 TO Y-1
64: END
```

C:\HYDRA\HEMET\LINE-Y20.CMD 17:10 22-May-..

------ S U M M A R Y O F A N A L Y S I S ------

Run number on command file :	1	
Number of links :	12	
Number of hydrographs :	50	
Total sanitary population :	4850	
Total sanitary area :	234.60	Acres
Total storm area :	0.00	Acres
Number of pumps :	0	
Number of reservoirs :	0	
Number of diversion structures :	0	
Number of inlets :	0	
Length of new pipe :	0.00	Feet
Length of existing pipe :	2616.06	Feet
Length of channel :	0.00	Feet
Length of gutter :	0.00	Feet
Length of transport units :	0.00	Feet
Length of pressure pipe :	0.00	Feet

C:\HYDRA\HEMET\LINE-Y20.CMD 17:10 22-May-90

LINE Y AT STETSON & PALM

*** THORNTON LATERAL Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
1	335	10	560.07	0.0031	0.5	0.0	2.02	0.46	58.92		
			559.03		0.0	0.0	0.62		0.78		
2	225	10	559.03	0.0026	0.5	0.0	1.90	0.46	64.11		
			558.44		0.0	0.0	0.66		0.72		
3	100	10	558.44	0.0032	0.5	0.0	2.12	0.53	66.14		
			558.12		0.0	0.0	0.67		0.79		
4	321	10	558.12	0.0028	0.5	0.0	2.03	0.53	70.27		
			557.21		0.0	0.0	0.70		0.75		
5	335	10	557.21	0.0028	0.5	0.0	2.02	0.53	71.01		
			556.28		0.0	0.0	0.70		0.74		
6	346	10	556.28	0.0023	0.7	0.0	1.99	0.71	106.37	0.04	8
			555.50		0.0	0.0	0.90		0.67		18
7	91	10	555.50	0.0032	0.7	0.0	2.32	0.72	91.07		
			555.21		0.0	0.0	0.83		0.79		
8	155	10	555.21	0.0030	0.7	0.0	2.25	0.72	94.40		
			554.75		0.0	0.0	0.86		0.77		
9	216	10	554.75	0.0024	0.7	0.0	2.05	0.73	106.25	0.04	8
			554.23		0.0	0.0	0.90		0.69		18
10	68	10	554.23	0.0028	0.7	0.0	2.21	0.73	98.61		
			554.04		0.0	0.0	0.90		0.74		
11	200	10	554.04	0.0028	0.7	0.0	2.21	0.74	100.01	0.00	8
			553.48		0.0	0.0	0.90		0.74		18
12	224	10	553.48	0.0099	0.8	0.0	3.55	0.78	55.83		
			551.26		0.0	0.0	0.60		1.40		

Lateral length= 2616 Upstream length= 2616

C:\HYDRA\HEMET\LINEBB20.CMD 17:11 22-May

Status of DEFAULTS at start of run. (* May be reset by SET)

Command file	C:\HYDRA\HEMET\LINEBB20.CMD
Input units are read as	USA
* Output sent to display	Brief
* Output sent to printer	Brief
* Output sent to file	Off
Paper width in inches	8.000
String to reset printer	27 38 108 54 68 27 40 115 49 48 72
String to set printer to compressed	17.16 27 38 107 48 56 72
String to set printer to 8 lines/inch	8 27 38 108 56 68
Name of printer	Hewlett-Packard, LaserJet/LaserJet P
Print heading at top of page	True
Number of steps in hydrograph	96
Step length in minutes	15
Significant flow in hydrograph	0.010
* Maximum plot value	Selected by HYDRA
Type of hydrographic plot	Compact
Sanitary flow by	Diurnal Curve
Delay to start of actual storm	0.00
Rational Method computations	Off
SCS computations	Santa Barbara
Continuous simulation computations	On
* Maximum d/D for pipe design/analysis	0.900
* Match point position on pipe	0.00 or Invert
* Number of allowable diam drops	999
* Mimimum drop thru manhole	0.000
Routing technique	Quick
* Calculate sanitary flows	True
* Calculate infiltration flows	True
* Calculate storm flows	True
* Calculate misc flows	True

```
 1: JOB LINE BB AT MENLO & LYON
 2: REM --- PIPE AND PIPE COST DATA ---
 3: PDA .013 8 8 7.5 3 .004
 4: CST 1.5 1 3 / .2 .5 .5 2.87 / .5 0 1.63 +
 5:         1.15 / .89 1.1 1.43 4.78
 6: EXC 0/.45  18/.45  30/1.12
 7: TSL 0/0  6/0  6.001/.5  30/.5
 8: PCO 8/2.78  10/4.10  18/9.16  36/18.23
 9: REM --- SANITARY CRITERIA ---
10: GPC 100          ! AVERAGE DAILY FLOW PER CAPITA
11: REM THIS MODEL RUN IS FOR 2010 CONDITIONS
12: REM THE FOLLOWING IS GHOST SYSTEM UPSTREAM OF M.H. BB-2
13: NEW SAN VICENTE DRIVE
```

C:\HYDRA\HEMET\LINEBB20.CMD 17:11 22-May-90

```
14: REM THE FOLLOWING IS BASED ON DIURNAL CURVE OF M.H.2 (R-A)
15: DIU 77.49 64.76 57.03 54.49 60.76 85.05 156.93 223.39 +
16:          233.46 238.6 224.07 204.05 182.09 172.48 170.59 158.67 +
17:          172 187.58 199.57 195.87 179.75 155.25 129.62 108.13
18: SAN 3.8  8.8  9.4! AREA TAKES 9.4 MIN. TO REACH OUR PIPE
19: SAN 5.7  8.8  6.1
20: SAN 2.0  8.8  2.8
21: PIP 1.0  551.05  551.05  543.68  543.68  -8! THIS IS A DUMMY PIPE
22: HOL SAN VICENTE
23: REM THE FOLLOWING IS GHOST UPSTREAM OF BB-1
24: NEW SONORA DRIVE
25: REM USE SAME DIURNAL CURVE
26: SAN 3.8  8.8
27: SAN 4.1  8.8
28: SAN 2.2  8.8
29: SAN 3.0  8.8
30: SAN 4.3  8.8
31: SAN 2.0  8.8
32: SAN 3.9  8.8
33: PIP 1.0  549.98  549.98  542.20  542.20  -8 ! THIS IS DUMMY ALSO
34: HOL SONORA
35: NEW OAKLAND AVE
36: REM THE FOLLOWING IS BASED ON DIURNAL CURVE OF M.H.5 (R-1)
37: DIU 53.67 46.85 44.76 48.62 65.47 108.26 159.47 172.14 167.55 +
38:          166.67 156.81 134.83 138.13 141.07 118.64 131.29 139.26 +
39:          156.17 155.95 143.65 127.75 104.19 87.91 67.28
40: REM THE FOLLOWING ARE GHOST UPSTREAM SYSTEMS
41: SAN 6.9  19.6   9.0! AREA TAKES 9 MIN. TO REACH OUR PIPE
42: SAN 3.4  37.4   5.6
43: SAN 4.6  20.8   2.2
44: SAN 6.6  15.4  12.8
45: SAN 7.3  37.4   8.3
46: SAN 5.9  37.4   4.7
47: SAN 7.7  37.4   5.0
48: PIP 330  558.90  557.36  551.58  550.26  -8!
49: REM THE REST IS BASED ON DIURNAL CURVE OF M.H.2 (R-A)
50: DIU 77.49 64.76 57.03 54.49 60.76 85.05 156.93 223.39 +
51:          233.46 238.6 224.07 204.05 182.09 172.48 170.59 158.67 +
52:          172 187.58 199.57 195.87 179.75 155.25 129.62 108.13
53: PIP 325  557.36  555.99  550.26  548.96  -8 ! BB-7 TO BB-6
54: SAN 12.1  20.7
55: PIP 325  555.99  554.63  548.96  547.66  -8 ! BB-6 TO BB-5
56: PIP 344  554.63  553.25  547.66  546.28  -8 ! BB-5 TO BB-4
57: SAN 11.9  8.8 ! INTERSECTION OF LYON AVE
58: PIP 331  553.25  552.10  546.28  544.95  -8 ! BB-4 TO BB-3
59: SAN 2.0  8.8
60: PIP 318  552.10  5551.05  544.95  543.68  -8 ! BB-3 TO BB-2
61: SAN 2.0  8.8
62: REC SAN VICENTE
63: PIP 368.4  551.05  549.98  543.63  542.20  -8 ! BB-2 TO BB-1
64: SAN 4.0  8.8
65: REC SONORA
```

C:\HYDRA\HEMET\LINEBB20.CMD 17:11 22-May-90

------ S U M M A R Y O F A N A L Y S I S ------

Run number on command file	:	1	
Number of links	:	10	
Number of hydrographs	:	46	
Total sanitary population	:	1973	
Total sanitary area	:	109.20	Acres
Total storm area	:	0.00	Acres
Number of pumps	:	0	
Number of reservoirs	:	0	
Number of diversion structures	:	0	
Number of inlets	:	0	
Length of new pipe	:	0.00	Feet
Length of existing pipe	:	2638.00	Feet
Length of channel	:	0.00	Feet
Length of gutter	:	0.00	Feet
Length of transport units	:	0.00	Feet
Length of pressure pipe	:	0.00	Feet

LINE BB AT MENLO & LYON

*** SAN VICENTE DRIVE — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
1	1	8	543.68	0.0000	0.0	0.0	0.00	0.02	999.99	0.00	0
			543.68		0.0	0.0	0.00		0.00		0

Lateral length= 1 Upstream length= 1

*** SONORA DRIVE — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
2	1	8	542.20	0.0000	0.0	0.0	0.00	0.03	999.99	0.00	0
			542.20		0.0	0.0	0.00		0.00		0

Lateral length= 1 Upstream length= 1

*** OAKLAND AVE — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
3	330	8	551.58	0.0040	0.2	0.0	1.71	0.18	36.90		
			550.26		0.0	0.0	0.48		0.49		
4	325	8	550.26	0.0040	0.2	0.0	1.71	0.18	36.90		
			548.96		0.0	0.0	0.48		0.49		
5	325	8	548.96	0.0040	0.2	0.0	1.81	0.22	44.32		
			547.66		0.0	0.0	0.53		0.49		
6	344	8	547.66	0.0040	0.2	0.0	1.81	0.22	44.26		
			546.28		0.0	0.0	0.53		0.49		
7	331	8	546.28	0.0040	0.2	0.0	1.85	0.23	47.46		
			544.95		0.0	0.0	0.55		0.49		
8	318	8	544.95	0.0040	0.2	0.0	1.85	0.24	48.11		
			543.68		0.0	0.0	0.55		0.49		
9	368	8	543.63	0.0039	0.3	0.0	1.88	0.25	52.45		
			542.20		0.0	0.0	0.58		0.48		

C:\HYDRA\HEMET\LINEBB20.CMD
17:11 22-May-90

LINE BB AT MENLO & LYON

*** OAKLAND AVE
Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
10	295	8	542.20	0.0040	0.3	0.0	1.97	0.29	59.34		
			541.03		0.0	0.0	0.63		0.49		
	Lateral length= 2636				Upstream length= 2638						

Status of DEFAULTS at start of run. (* May be reset by SET)

```
|
|  Command file : C:\HYDRA\HEMET\LINE_BB.CMD
|  Input units are read as                 : USA
|* Output sent to display                  : Brief
|* Output sent to printer                  : Brief
|* Output sent to file                     : Off
|  Paper width in inches                   : 8.000
|  String to reset printer                 : 27 38 108 54 68 27 40 115 49 48 72
|  String to set printer to compressed     : 17.16 27 38 107 48 56 72
|  String to set printer to 8 lines/inch   : 8 27 38 108 56 68
|  Name of printer                         : Hewlett-Packard, LaserJet/LaserJet
|  Print heading at top of page            : True
|
|  Number of steps in hydrograph           : 96
|  Step length in minutes                  : 15
|  Significant flow in hydrograph          : 0.010
|* Maximum plot value                      : Selected by HYDRA
|  Type of hydrographic plot               : Compact
|
|  Sanitary flow by                        : Diurnal Curve
|  Delay to start of actual storm          : 0.00
|  Rational Method computations            : Off
|  SCS computations                        : Santa Barbara
|  Continuous simulation computations      : On
|
|* Maximum d/D for pipe design/analysis    : 0.900
|* Match point position on pipe            : 0.00 or Invert
|* Number of allowable diam drops          : 999
|* Mimimum drop thru manhole               : 0.000
|  Routing technique                       : Quick
|
|* Calculate sanitary flows                : True
|* Calculate infiltration flows            : True
|* Calculate storm flows                   : True
|* Calculate misc flows                    : True
|
+-------------------------------------------------------------------
```

```
 1: JOB LINE BB AT MENLO & LYON
 2: REM --- PIPE AND PIPE COST DATA ---
 3: PDA .013 8 8 7.5 3 .004
 4: CST 1.5 1 3 / .2 .5 .5 2.87 / .5 0 1.63 +
 5:          1.15 / .89 1.1 1.43 4.78
 6: EXC 0/.45  18/.45  30/1.12
 7: TSL 0/0  6/0  6.001/.5  30/.5
 8: PCO 8/2.78  10/4.10  18/9.16  36/18.23
 9: REM --- SANITARY CRITERIA ---
10: GPC 100           ! AVERAGE DAILY FLOW PER CAPITA
11: REM THIS MODEL RUN IS FOR 1990 CONDITIONS
12: REM THE FOLLOWING IS GHOST SYSTEM UPSTREAM OF M.H. BB-2
13: NEW SAN VICENTE DRIVE
```

C:\HYDRA\HEMET\LINE_BB.CMD 17:12 22-May-90

```
14: REM THE FOLLOWING IS BASED ON DIURNAL CURVE OF M.H.2 (R-A)
15: DIU 77.49 64.76 57.03 54.49 60.76 85.05 156.93 223.39 +
16:          233.46 238.6 224.07 204.05 182.09 172.48 170.59 158.67 +
17:          172 187.58 199.57 195.87 179.75 155.25 129.62 108.13
18: SAN 3.8  7.7  9.4! AREA TAKES 9.4 MIN. TO REACH OUR PIPE
19: SAN 5.7  7.7  6.1
20: SAN 2.0  7.7  2.8
21: PIP 1.0  551.05  551.05  543.68  543.68  -8! THIS IS A DUMMY PIPE
22: HOL SAN VICENTE
23: REM THE FOLLOWING IS GHOST UPSTREAM OF BB-1
24: NEW SONORA DRIVE
25: REM USE SAME DIURNAL CURVE
26: SAN 3.8  7.7
27: SAN 4.1  7.7
28: SAN 2.2  7.7
29: SAN 3.0  7.7
30: SAN 4.3  7.7
31: SAN 2.0  7.7
32: SAN 3.9  7.7
33: PIP 1.0  549.98  549.98  542.20  542.20  -8 ! THIS IS DUMMY ALSO
34: HOL SONORA
35: NEW OAKLAND AVE
36: REM THE FOLLOWING IS BASED ON DIURNAL CURVE OF M.H.5 (R-1)
37: DIU 53.67 46.85 44.76 48.62 65.47 108.26 159.47 172.14 167.55 +
38:          166.67 156.81 134.83 138.13 141.07 118.64 131.29 139.26 +
39:          156.17 155.95 143.65 127.75 104.19 87.91 67.28
40: REM THE FOLLOWING ARE GHOST UPSTREAM SYSTEMS
41: SAN 6.9  16.5   9.0! AREA TAKES 9 MIN. TO REACH OUR PIPE
42: SAN 3.4  27.4   5.6
43: SAN 4.6  16.9   2.2
44: SAN 6.6  13.4  12.8
45: SAN 7.3  27.7   8.3
46: SAN 5.9  27.4   4.7
47: SAN 7.7  27.4   5.0
48: PIP 330  558.90  557.36  551.58  550.26  -8!
49: REM THE REST IS BASED ON DIURNAL CURVE OF M.H.2 (R-A)
50: DIU 77.49 64.76 57.03 54.49 60.76 85.05 156.93 223.39 +
51:          233.46 238.6 224.07 204.05 182.09 172.48 170.59 158.67 +
52:          172 187.58 199.57 195.87 179.75 155.25 129.62 108.13
53: PIP 325  557.36  555.99  550.26  548.96  -8 ! BB-7 TO BB-6
54: SAN 12.1  16.8
55: PIP 325  555.99  554.63  548.96  547.66  -8 ! BB-6 TO BB-5
56: PIP 344  554.63  553.25  547.66  546.28  -8 ! BB-5 TO BB-4
57: SAN 11.9  7.7 ! INTERSECTION OF LYON AVE
58: PIP 331  553.25  552.10  546.28  544.95  -8 ! BB-4 TO BB-3
59: SAN 2.0  7.7
60: PIP 318  552.10  5551.05  544.95  543.68  -8 ! BB-3 TO BB-2
61: SAN 2.0  7.7
62: REC SAN VICENTE
63: PIP 368.4  551.05  549.98  543.63  542.20  -8 ! BB-2 TO BB-1
64: SAN 4.0  7.7
65: REC SONORA
```

```
 66: PIP 294.6  549.98  549.00  542.20  541.03  -8 ! BB-1 TO BB
 67: END
```

\HYDRA\HEMET\LINE_BB.CMD
17:12 22-May-90

------ S U M M A R Y O F A N A L Y S I S ------

Run number on command file :	1	
Number of links :	10	
Number of hydrographs :	46	
Total sanitary population :	1573	
Total sanitary area :	109.20	Acres
Total storm area :	0.00	Acres
Number of pumps :	0	
Number of reservoirs :	0	
Number of diversion structures :	0	
Number of inlets :	0	
Length of new pipe :	0.00	Feet
Length of existing pipe :	2638.00	Feet
Length of channel :	0.00	Feet
Length of gutter :	0.00	Feet
Length of transport units :	0.00	Feet
Length of pressure pipe :	0.00	Feet

LINE BB AT MENLO & LYON

*** SAN VICENTE DRIVE — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
1	1	8	543.68	0.0000	0.0	0.0	0.00	0.01	999.99	0.00	0
			543.68		0.0	0.0	0.00		0.00		0

Lateral length= 1 Upstream length= 1

*** SONORA DRIVE — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
2	1	8	542.20	0.0000	0.0	0.0	0.00	0.03	999.99	0.00	0
			542.20		0.0	0.0	0.00		0.00		0

Lateral length= 1 Upstream length= 1

*** OAKLAND AVE — Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
3	330	8	551.58	0.0040	0.1	0.0	1.58	0.14	28.18		
			550.26		0.0	0.0	0.41		0.49		
4	325	8	550.26	0.0040	0.1	0.0	1.58	0.14	28.18		
			548.96		0.0	0.0	0.41		0.49		
5	325	8	548.96	0.0040	0.2	0.0	1.67	0.17	34.22		
			547.66		0.0	0.0	0.46		0.49		
6	344	8	547.66	0.0040	0.2	0.0	1.67	0.17	34.17		
			546.28		0.0	0.0	0.46		0.49		
7	331	8	546.28	0.0040	0.2	0.0	1.72	0.18	36.97		
			544.95		0.0	0.0	0.48		0.49		
8	318	8	544.95	0.0040	0.2	0.0	1.72	0.18	37.53		
			543.68		0.0	0.0	0.48		0.49		
9	368	8	543.63	0.0039	0.2	0.0	1.74	0.20	41.27		
			542.20		0.0	0.0	0.51		0.48		

C:\HYDRA\HEMET\LINE_BB.CMD
17:13 22-May-90

LINE BB AT MENLO & LYON

*** OAKLAND AVE
Analysis of Existing Pipes

Link	Long	Diam	Invert Up/Dn	Slope	San Inf	Sto Mis	Vel d/D	Design MGD	% Cap Q Full	Remove	Par Rep
10	295	8	542.20	0.0040	0.2	0.0	1.84	0.23	47.34		
			541.03		0.0	0.0	0.55		0.49		

Lateral length= 2636 Upstream length= 2638